

# Sludge Sedimentation Basins Inflow Design Flood Control System Plan

**Clover Power Station  
Clover, Virginia**

October 2021



Jonathan Hotstream  
Senior Scientist

**Prepared For:**

Virginia Electric and Power Company  
4091 Clover Road  
Clover, Virginia 24534

**Prepared By:**

TRC  
50 International Drive, Suite 150  
Greenville, South Carolina 29615



Nakia Addison, P.E.  
Project Manager



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## Revision History

Revision Number	Revision Date	Section Revised	Summary of Revisions
0	10/3/2016		Initial Issue
1	10/14/2021	1, 2, 3, App. A and C	Periodic 5-year revision.

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## 1.0 Background

Virginia Electric and Power Company d/b/a Dominion Virginia Power (Dominion) owns<sup>1</sup> and operates the Clover Power Station. The purpose of this Inflow Design Flood Control System Plan (Plan) is to present the flood control features of the two retrofitted sludge sedimentation basins at the Clover Power Station. These two basins are managed in a manner that controls the inflow design flood, as required by the United States Environmental Protection Agency's (USEPA) final coal combustion residuals (CCR) rule, Title 40 Code of Federal Regulations (40 CFR) Part 257 Subpart D - "Standards for the Disposal of Coal Combustion Residuals in Landfills and Surface Impoundments." The basins are considered existing surface impoundments according to the CCR rule (40 CFR 257.53).

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<sup>1</sup> Old Dominion Electric Cooperative owns a 50% undivided interest in the Clover Power Station.

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## 2.0 Inflow Design Flood Control

Hydrologic and hydraulic capacity requirements for CCR surface impoundments are set forth in 40 CFR 257.82. The sludge sedimentation basins are classified as Low Hazard in accordance with 40 CFR 57.73 and 40 CFR 257.74. Based on the Low Hazard potential classification, the CCR unit must adequately manage flow into the unit during and following the peak discharge of the 100-year flood (40 CFR 257.82(a)(3)(iii)).

The sludge sedimentation basins were designed in accordance with 40 CFR 257.82(a)(1), (2) and (3), requiring the CCR units to adequately manage inflows during and following peak discharge and to manage outflows to collect and control peak discharge for a 100-year flood due to the Low Hazard classification.

The Flood Insurance Rate Map for the Clover Power Station (National Flood Insurance Program 2009) indicates that the basins are located in an area determined to be outside the 0.2% annual chance flood, refer to Appendix B. Figures 1 and 2 show the extents of the 100-year flood. The basins are located in an area that is above the 100-year flood elevation; therefore, the basins will not experience surface water inflow during the design flood event. The basins have been designed with several inflow features presented in the sections below to mitigate and control floods.

### 2.1 Basin Operation

The sludge sedimentation basins are utilized for managing Station low volume process wastewaters. The basins are operated in parallel. Both basins are typically active and available to receive low volume wastewaters from the Station. As needed, accumulated solids are dewatered, removed, and transported to the Station's CCR landfill for disposal. The basins were designed to operate with freeboard, height difference from the top of the berm to the water level, to provide additional short-term storage in the basins.

The water level in the active basin is monitored by level transmitters located in the pump station wet well and during weekly visual inspections. The pump system is programmed to remove water from the basin based on high and low level switches. In addition to level switches, there are high and low level alarms that notify control operators in the Station of needed action.

The following control measures are implemented during basin operation to control the water levels in the basins:

- Operate the basins in parallel during typical operations. The system has the ability to operate the basins independently and isolate each basin for operation, maintenance and cleaning. Based on this use pattern, only one basin is at the operating water level at a time.
- Operate pumps as needed to control the basin water levels.
- Regularly check and maintain grades surrounding the basins to minimize the area contributing to storm water run-on.

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## 2.2 Run-on Control

The basins were designed to control the storm water run-on from a 100-year, 24-hour storm event based upon the Precipitation Frequency Estimates from the National Oceanic and Atmospheric Administration. The storm water run-on volume calculated for the design storm was compared to the storage capacity above the operating water elevation. The evaluation determined that there is sufficient capacity in the basins when operating with 1.5 feet of freeboard, refer to Appendix C.

## 2.3 Pumping Capacity

The pump station is equipped with two Lawrence VPL3200 pumps with a rated pumping capacity of 410 gallons per minute (gpm) at 110 feet of head. The two pump configuration provides a duty pump and a backup pump in the event of malfunction, maintenance, or repair of the duty pump. A calculation was performed to determine the length of time required to remove the anticipated run-on due to a 100-year, 24-hour storm event, refer to Appendix B. The calculation was performed using only the capacity of the duty pump and resulted in a required time of 51 hours or approximately 2 days to remove the anticipated storm water run-on from both basins. This calculation shows that pumping rates are sufficient in controlling water levels in the basins.

## 2.4 Conclusions

The basins meet the requirements of 40 CFR 257.82 of adequately controlling the inflows and outflows of peak discharge at the Clover Power Station for the following reasons:

- The basins are located above the 100-year floodplain.
- The basins were adequately designed to manage precipitation volumes resulting from a 100-year, 24-hour storm event.
- The pumping rates are sufficient to control the water levels in both basins.

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### 3.0 Amendment and Periodic Plan Revision

This Plan has been completed in compliance with the requirements set forth in 40 CFR 257.82. This document will be placed in the Station's CCR operating record, posted to the publicly accessible CCR website, and government notifications will be provided.

A periodic inflow design flood control system plan must be prepared every 5 years from the completion date of this Plan. The next Plan update is required by October 2026.

The Plan must be amended whenever the periodic review period is reached or if changes in site conditions occur that will sustainably affect the current written Plan.

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## 4.0 References

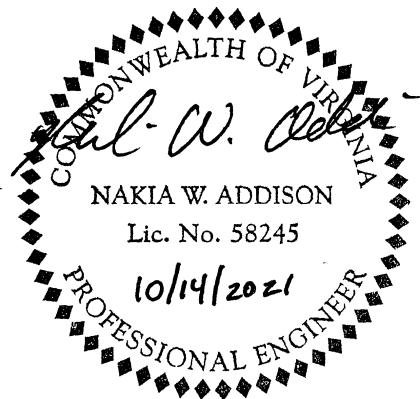
TRC Engineers, Inc. 2021. Initial Hazard Potential Classification – Sludge Sedimentation Basins Clover Power Station. October 2021.

National Flood Insurance Program. 2009. Flood Insurance Rate Map: Halifax County Virginia Panel 350 of 625. Map Number 51083C0350D. Effective Date October 16, 2009. Federal Emergency Management Agency. Washington, D.C.

## 5.0 Certification

I, the undersigned Virginia Professional Engineer, hereby certify that I am familiar with the technical requirements of 40 CFR 257 Subpart D. I also certify that it is my professional opinion that, to the best of my knowledge, information, and belief, that the information in this demonstration is in accordance with current good and accepted engineering practice(s) and standard(s) and meets the requirements of paragraph (a) of in 40 CFR 257.82.

For the purpose of this document, "certify" and "certification" shall be interpreted and construed to be a "statement of professional opinion." The certification is understood and intended to be an expression of my professional opinion as a Virginia Licensed Professional Engineer, based upon knowledge, information, and belief. The statement(s) of professional opinion are not and shall not be interpreted or construed to be a guarantee or a warranty of the analysis herein.



Nakia Addison, P.E.

Printed Name of Professional Engineer

58245

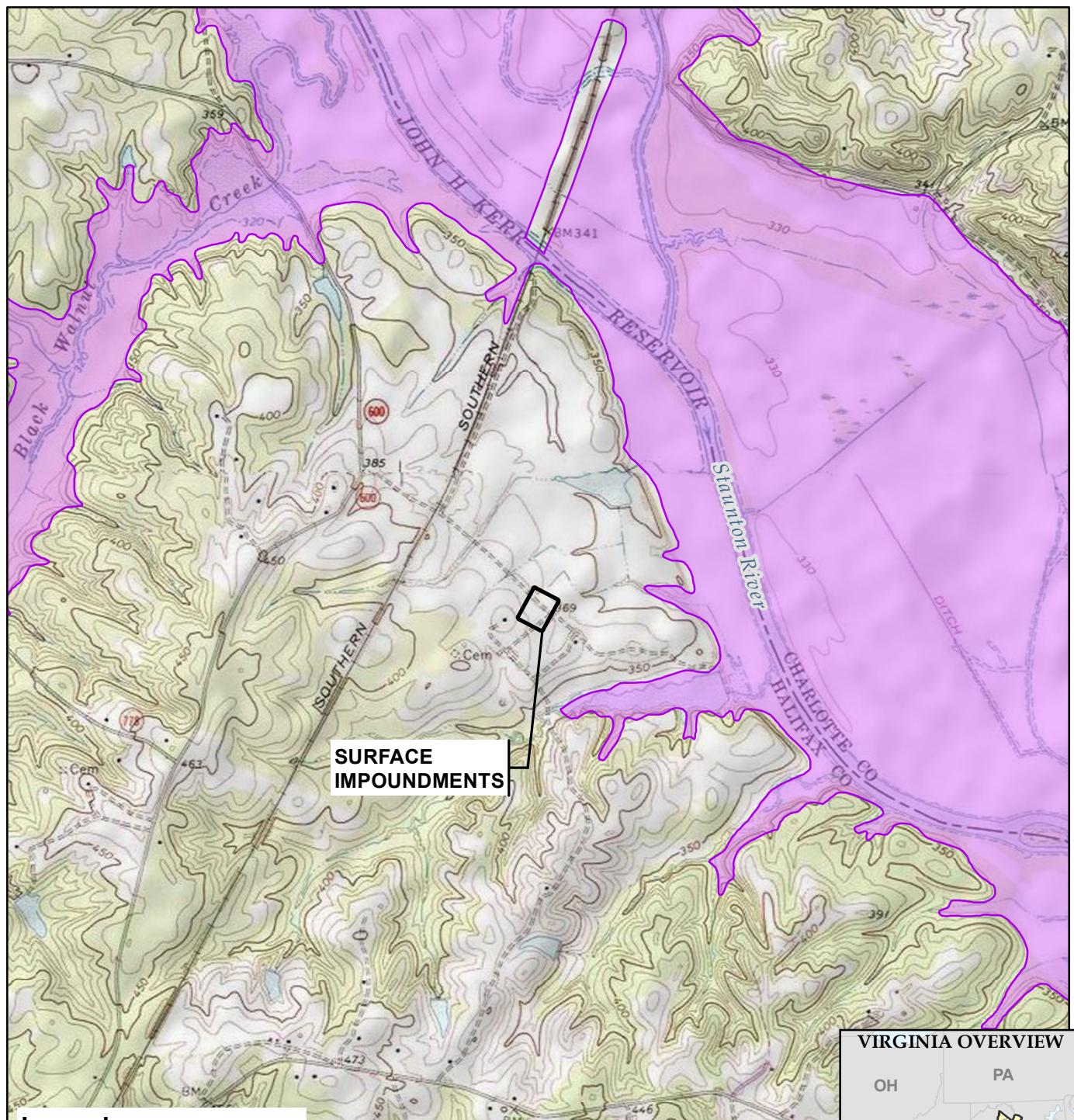
Commonwealth of Virginia License Number



Signature of Professional Engineer

October 14, 2021

Date

**Legend**

EXTENTS OF 100-YEAR FLOODPLAIN

**VIRGINIA OVERVIEW**

-BASE MAP FROM USGS 7.5 MINUTE TOPOGRAPHIC QUADRANGLE SERIES, 1982.  
-FLOOD DATA ACQUIRED FROM FEMA NATIONAL FLOOD HAZARD LAYER (NFHL).

1" = 2,000' 0 2,000 4,000 FEET  
1:24,000

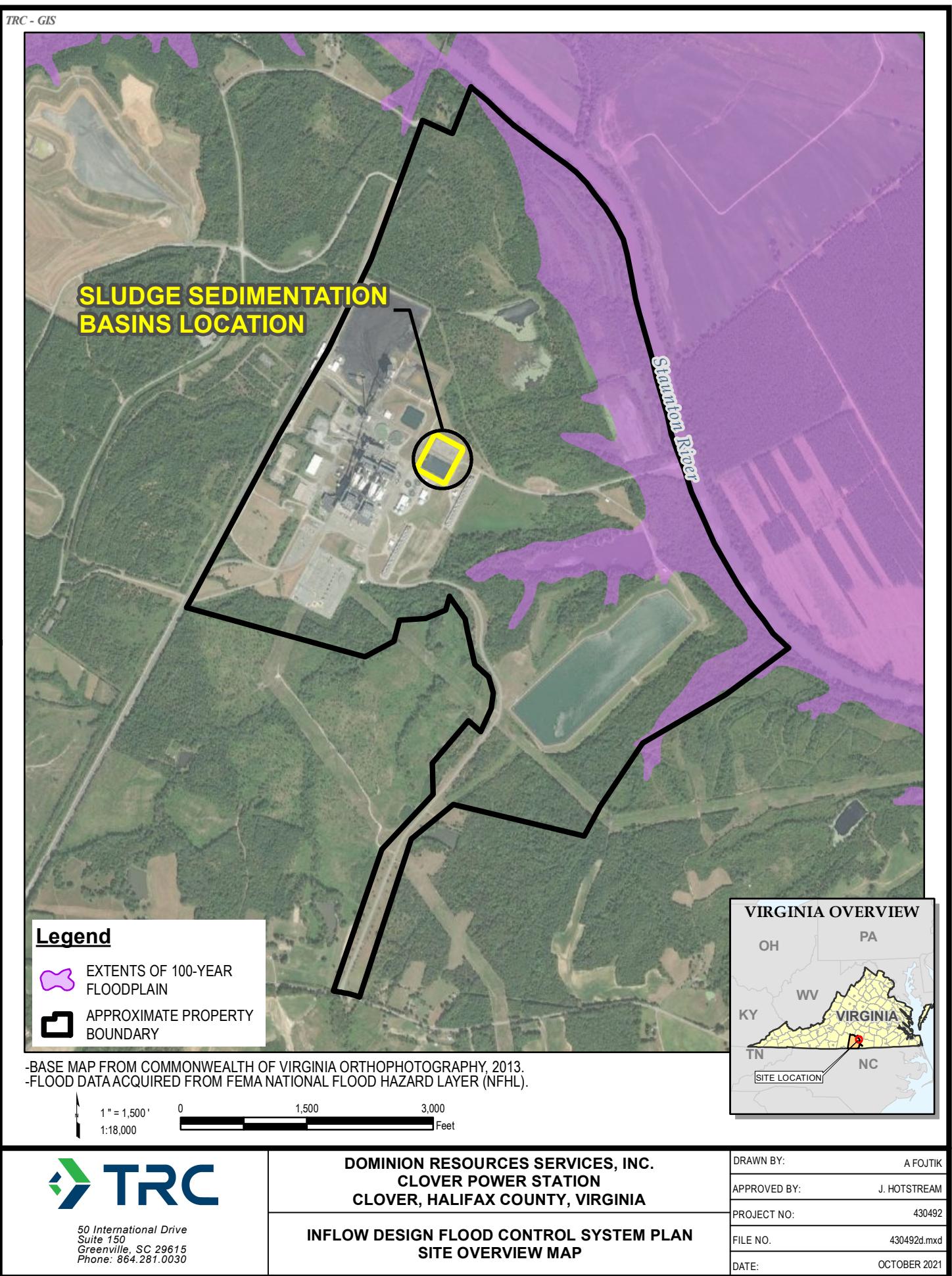


50 International Drive  
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Phone: 864.281.0030

**DOMINION RESOURCES SERVICES, INC.  
CLOVER POWER STATION  
CLOVER, HALIFAX COUNTY, VIRGINIA**

**INFLOW DESIGN FLOOD CONTROL SYSTEM PLAN  
SITE LOCATION MAP**

DRAWN BY:	A FOJTIK
APPROVED BY:	J. HOTSTREAM
PROJECT NO:	430492
FILE NO.	430492c.mxd
DATE:	OCTOBER 2021





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## Appendix A: Selected Retrofit Design Drawings

# CLOVER POWER STATION

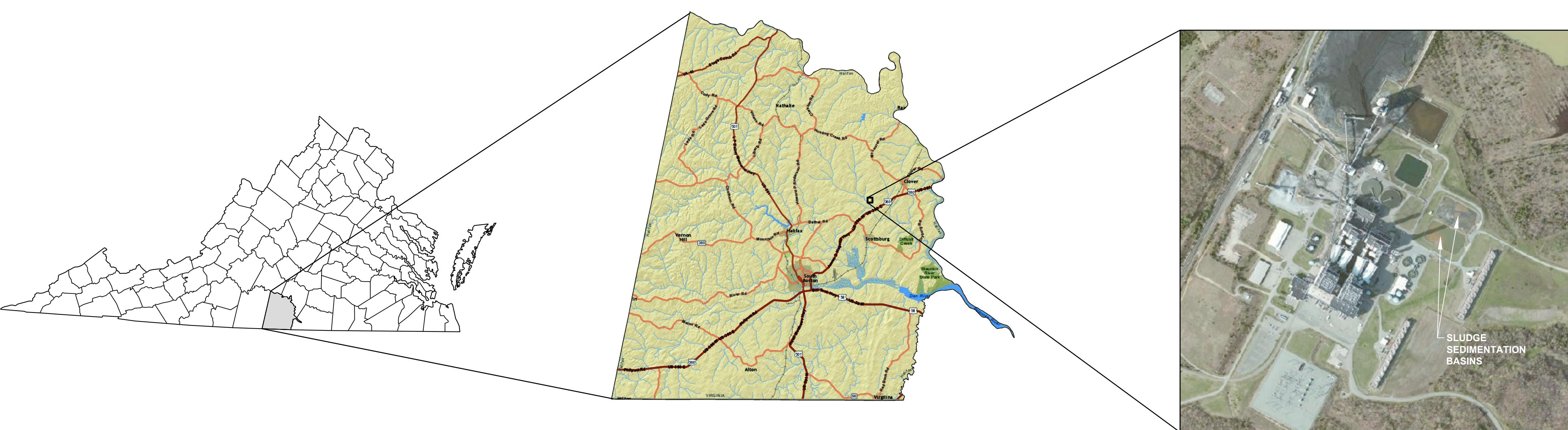
# RETROFIT - SLUDGE SEDIMENTATION BASINS

# AS-BUILT DRAWINGS

PREPARED FOR: DOMINION RESOURCES SERVICES, INC.  
CLOVER POWER STATION  
CLOVER, VIRGINIA

PREPARED BY: TRC ENGINEERS, INC.  
GREENVILLE, SOUTH CAROLINA

DATE: NOVEMBER 2016  
REVISED JULY 2017  
REVISED SEPTEMBER 2017  
REVISED SEPTEMBER 2019



VIRGINIA

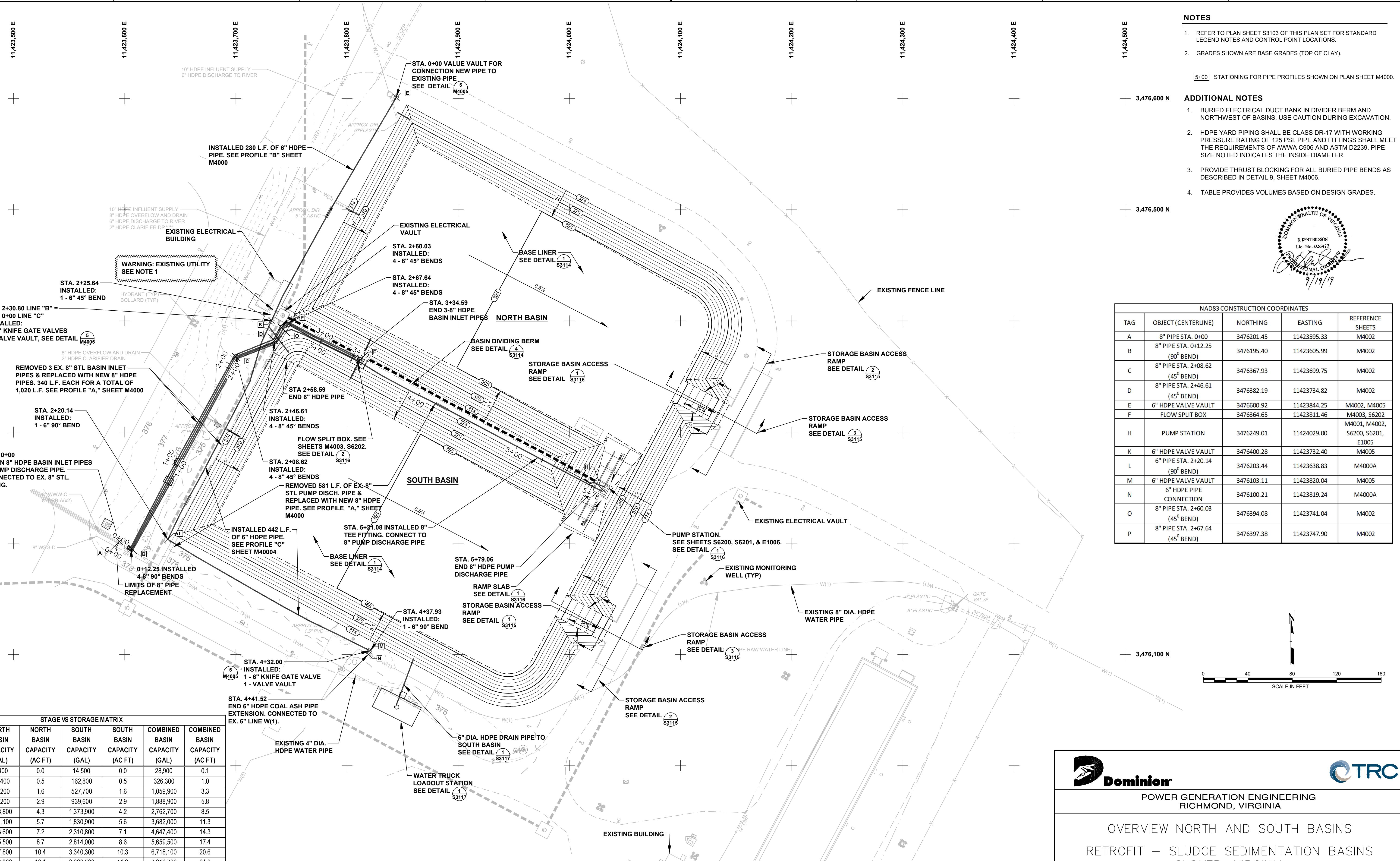
HALIFAX COUNTY

SITE LOCATOR

1" = 600'

SHEET INDEX		
SHEET NUMBER	SHEET TITLE	REVISION
66706-15348-CWSG-S3100	TITLE SHEET	
66706-15348-CWSG-S3101	GENERAL NOTES - CIVIL, MECHANICAL, STRUCTURAL	2
66706-15348-CWSG-S3102	GENERAL NOTES - CIVIL, MECHANICAL, STRUCTURAL	1
66706-15348-CWSG-S3103	CIVIL STANDARD LEGEND	5
66706-15348-CWSG-S3104	EXISTING CONDITIONS	3
66706-15348-CWSG-S3105	SUGGESTED CONSTRUCTION SEQUENCE PLAN	5
66706-15348-CWSG-S3106	EROSION AND SEDIMENT CONTROL PLAN	5
66706-15348-CWSG-S3107	OVERVIEW NORTH AND SOUTH BASINS	5
66706-15348-CWSG-S3108	NORTH BASIN LINER SUBBASE GRADES	5
66706-15348-CWSG-S3108B	NORTH BASIN LINER BASE GRADES	5
66706-15348-CWSG-S3108C	NORTH BASIN PANEL LAYOUT	2
66706-15348-CWSG-S3109	NORTH BASIN BASE AND PAVING	5
66706-15348-CWSG-S3110	NORTH BASIN CROSS SECTIONS	2
66706-15348-CWSG-S3111	SOUTH BASIN LINER SUBBASE GRADES	5
66706-15348-CWSG-S3111B	SOUTH BASIN LINER BASE GRADES	5
66706-15348-CWSG-S3111C	SOUTH BASIN PANEL LAYOUT	2
66706-15348-CWSG-S3112	SOUTH BASIN BASE AND PAVING	5
66706-15348-CWSG-S3113	SOUTH BASIN CROSS SECTIONS	3
66706-15348-CWSG-S3114	CIVIL DETAILS - NORTH AND SOUTH BASINS	5
66706-15348-CWSG-S3115	CIVIL DETAILS - NORTH AND SOUTH BASINS	5
66706-15348-CWSG-S3116	CIVIL DETAILS - SOUTH BASIN	3
66706-15348-CWSG-S3117	CIVIL DETAILS - SOUTH BASIN	5
66706-15348-CWSG-S3118	CIVIL DETAILS	5
66706-15348-CWSG-S3119	CIVIL DETAILS - EROSION AND SEDIMENT CONTROL	3
66706-15348-CWSG-M2647	MECHANICAL P&ID	1
66706-15348-CWSG-M4000	YARD PIPING PROFILES	2
66706-15348-CWSG-M4000A	YARD PIPING PROFILES	2
66706-15348-CWSG-M4001	PUMP STATION PLAN VIEW	1
66706-15348-CWSG-M4002	PUMP STATION SECTION VIEWS	1
66706-15348-CWSG-M4003	FLOW SPLIT BOX PLAN AND SECTIONS	1
66706-15348-CWSG-M4004	TEMPORARY PUMP STATION PLAN	1
66706-15348-CWSG-M4005	MECHANICAL DETAILS 1	1
66706-15348-CWSG-M4006	MECHANICAL DETAILS 2	1
66706-15348-CWSG-S6200	STRUCTURAL - SLUDGE PUMP STATION	1
66706-15348-CWSG-S6201	STRUCTURAL - SLUDGE PUMP STATION	1
66706-15348-CWSG-S6202	STRUCTURAL - FLOW SPLIT BOX	1
66706-15348-CWSG-S6203	STRUCTURAL - TYPICAL SECTIONS AND DETAILS	1
66706-15348-CWSG-S6204	STRUCTURAL/ARCHITECTURAL - SECTIONS & DETAILS	1
66706-15348-CWSG-E1001	ELECTRICAL SYMBOLS AND ABBREVIATIONS	1
66706-15348-CWSG-E1002	ELECTRICAL SITE PLAN - DEMO	1
66706-15348-CWSG-E1003	ELECTRICAL SITE PLAN - PROPOSED	1
66706-15348-CWSG-E1004	ELECTRICAL ONELINE	1
66706-15348-CWSG-E1005	ELECTRICAL DETAILS AND ENLARGED PLANS	1
66706-15348-CWSG-E1006	ELECTRICAL DETAILS	1
66706-15348-CWSG-E1007	ELECTRICAL DETAILS AND RACEWAY SCHEDULE	1
66706-15348-CWSG-E1008	CABLE AND PANEL SCHEDULE	1

COMMONWEALTH OF VIRGINIA  
R. KENT NILSSON  
Lic. No. 026477  
INTERNATIONAL ENGINEERS  
9/19/19



## OTES

- REFER TO PLAN SHEET S3103 OF THIS PLAN SET FOR STANDARD  
LEGEND NOTES AND CONTROL POINT LOCATIONS.

GRADES SHOWN ARE BASE GRADES (TOP OF CLAY).

+00 STATIONING FOR PIPE PROFILES SHOWN ON PLAN SHEET M4000

## ADDITIONAL NOTES

- BURIED ELECTRICAL DUCT BANK IN DIVIDER BERM AND  
NORTHWEST OF BASINS. USE CAUTION DURING EXCAVATION.**

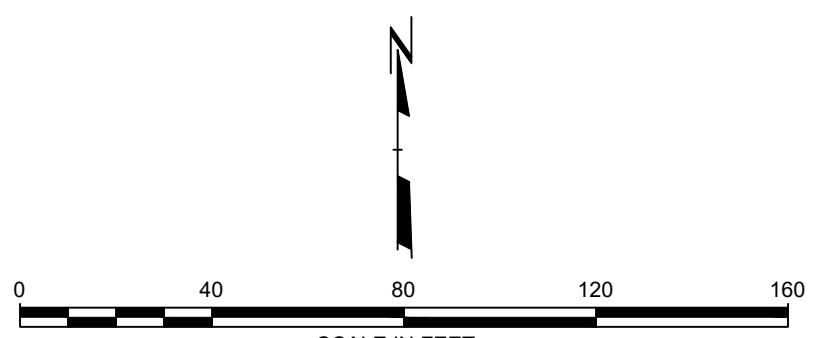
**HDPE YARD PIPING SHALL BE CLASS DR-17 WITH WORKING  
PRESSURE RATING OF 125 PSI. PIPE AND FITTINGS SHALL MEET  
THE REQUIREMENTS OF AWWA C906 AND ASTM D2239. PIPE  
SIZE NOTED INDICATES THE INSIDE DIAMETER.**

**PROVIDE THRUST BLOCKING FOR ALL BURIED PIPE BENDS AS  
DESCRIBED IN DETAIL 9, SHEET M4006.**

**TABLE PROVIDES VOLUMES BASED ON DESIGN GRADES.**

The circular seal features a diamond pattern border. The words "COMMONWEALTH OF VIRGINIA" are written along the top inner edge, and "PROFESSIONAL ENGINEER" are written along the bottom inner edge. In the center, it says "R. KENT NILSSON" above "Lic. No. 026477". At the bottom, there is a signature and the date "9/19/19".

NAD83 CONSTRUCTION COORDINATES				
AG	OBJECT (CENTERLINE)	NORTHING	EASTING	REFERENCE SHEETS
A	8" PIPE STA. 0+00	3476201.45	11423595.33	M4002
B	8" PIPE STA. 0+12.25 (90° BEND)	3476195.40	11423605.99	M4002
C	8" PIPE STA. 2+08.62 (45° BEND)	3476367.93	11423699.75	M4002
D	8" PIPE STA. 2+46.61 (45° BEND)	3476382.19	11423734.82	M4002
E	6" HDPE VALVE VAULT	3476600.92	11423844.25	M4002, M4005
F	FLOW SPLIT BOX	3476364.65	11423811.46	M4003, S6202
H	PUMP STATION	3476249.01	11424029.00	M4001, M4002, S6200, S6201, E1005
K	6" HDPE VALVE VAULT	3476400.28	11423732.40	M4005
L	6" PIPE STA. 2+20.14 (90° BEND)	3476203.44	11423638.83	M4000A
M	6" HDPE VALVE VAULT	3476103.11	11423820.04	M4005
N	6" HDPE PIPE CONNECTION	3476100.21	11423819.24	M4000A
O	8" PIPE STA. 2+60.03 (45° BEND)	3476394.08	11423741.04	M4002
P	8" PIPE STA. 2+67.64 (45° BEND)	3476397.38	11423747.90	M4002



## RICHMOND, VIRGINIA

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# OVERVIEW NORTH AND SOUTH BASINS

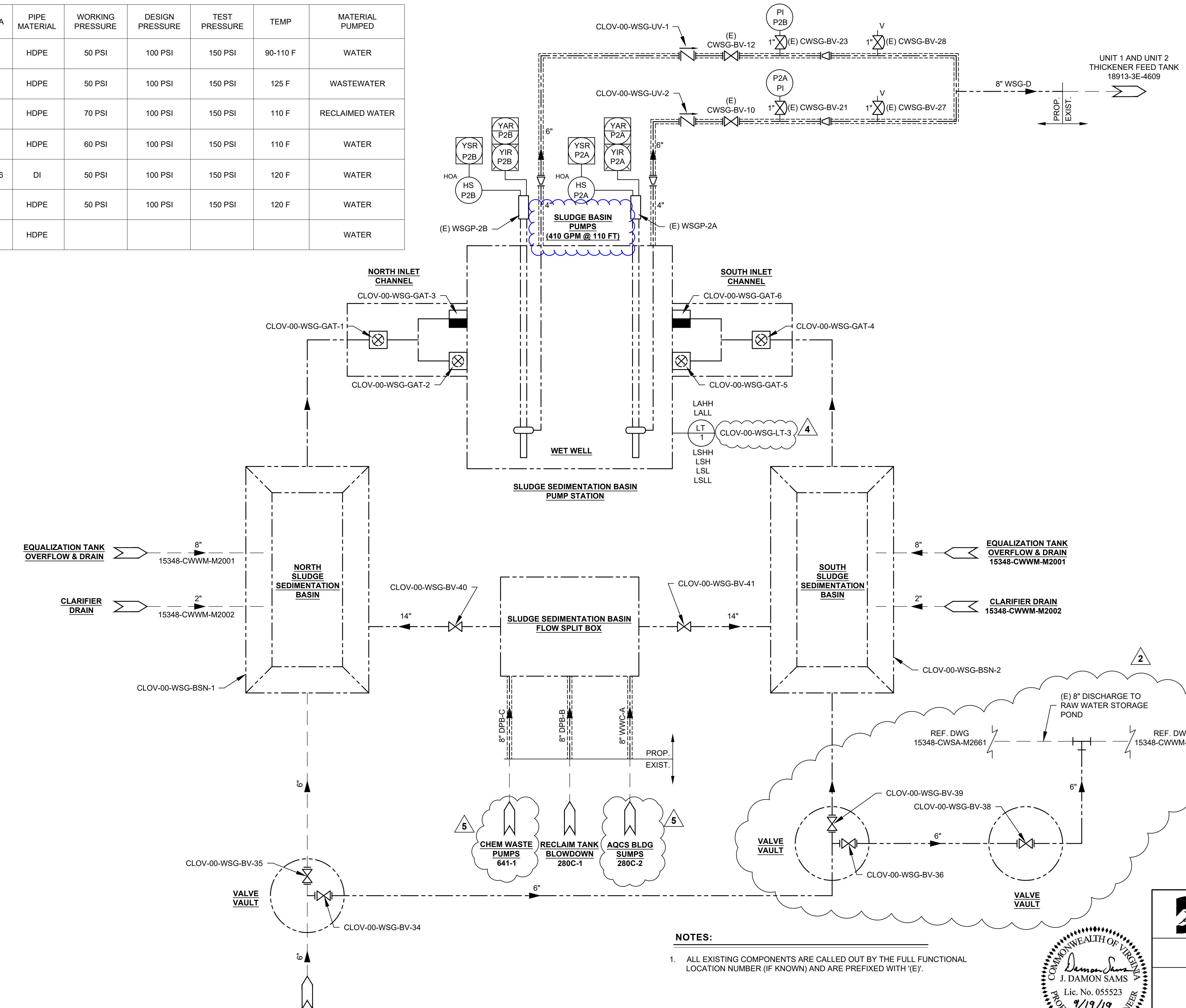
## METROFIT – SLUDGE SEDIMENTATION BASINS

STAGE VS STORAGE MATRIX						
ELEVATION	NORTH BASIN CAPACITY (GAL)	NORTH BASIN CAPACITY (AC FT)	SOUTH BASIN CAPACITY (GAL)	SOUTH BASIN CAPACITY (AC FT)	COMBINED BASIN CAPACITY (GAL)	COMBINE BASIN CAPACIT (AC FT)
365	14,400	0.0	14,500	0.0	28,900	0.1
366	163,400	0.5	162,800	0.5	326,300	1.0
367	532,200	1.6	527,700	1.6	1,059,900	3.3
368	949,200	2.9	939,600	2.9	1,888,900	5.8
369	1,388,800	4.3	1,373,900	4.2	2,762,700	8.5
370	1,851,100	5.7	1,830,900	5.6	3,682,000	11.3
371	2,336,600	7.2	2,310,800	7.1	4,647,400	14.3
372	2,845,500	8.7	2,814,000	8.6	5,659,500	17.4
373	3,377,800	10.4	3,340,300	10.3	6,718,100	20.6
374	3,920,200	12.1	3,906,500	11.9	7,816,700	24.0

## **LINE LIST:**

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LINE ID	DESC	DIA	PIPE MATERIAL	WORKING PRESSURE	DESIGN PRESSURE	TEST PRESSURE	TEMP	MATERIAL PUMPED
	FROM COAL POND TO SOUTH SLUDGE POND	6	HDPE	50 PSI	100 PSI	150 PSI	90-110 F	WATER
WWC-A	FROM CHEMICAL WASTE	8	HDPE	50 PSI	100 PSI	150 PSI	125 F	WASTEWATER
DPB-B	RECLAIM TANK BLOWDOWN	8	HDPE	70 PSI	100 PSI	150 PSI	110 F	RECLAIMED WATER
DPB-C	AQC BLDG SUMP PUMP DISCH	8	HDPE	60 PSI	100 PSI	150 PSI	110 F	WATER
WSG-D	SLUDGE STORAGE POND PUMP DISCHARGE (ABOVE GROUND)	4/6	DI	50 PSI	100 PSI	150 PSI	120 F	WATER
WSG-D	SLUDGE STORAGE POND PUMP DISCHARGE (BURIED)	8	HDPE	50 PSI	100 PSI	150 PSI	120 F	WATER
	DISCHARGE TO RAW WATER STORAGE POND(BURIED)	8	HDPE					WATER



## **LEGEND AND ABBREVIATIONS**

	EXISTING DEVICE		BUTTERFLY VALVE
	FIELD LOCATED DEVICE		MOTORIZED PLUG VALVE
	PANEL MOUNTED DEVICE		CHECK VALVE
	STATUS INDICATOR LIGHT		DIRECTION OF FLOW
	OPERATOR INTERFACE		CAP OR PLUG
	HAND-OFF-AUTO SWITCH		REDUCER
<hr style="border-top: 1px dashed black; margin-bottom: 10px;"/>			MIXER
<hr style="border-top: 1px dashed black; margin-bottom: 10px;"/>			SLIDE GATE
<hr style="border-top: 1px dashed black; margin-bottom: 10px;"/>			BALL VALVE
<hr style="border-top: 1px dashed black; margin-bottom: 10px;"/>			GATE VALVE
	FLOW CONTINUATION		PLUG VALVE
	FLOW CONTINUATION ON THIS SHEET		DIAPHRAGM VALVE
	AIR RELEASE VALVE		WEIR GATE
	SUBMERSIBLE PUMP		MANHOLE
	CENTRIFUGAL PUMP		JACKETED PIPE

ALYZER ALARM HIGH	PI	PRESSURE INDICATOR
ALYZER ALARM LOW	PIV	PRESSURE INDICATOR-VACUUM
ALYZER INDICATOR	PSV	PRESSURE SAFETY VALVE
ALYZER INDICATOR/	TAH	TEMP. ALARM HIGH
ANSMITTER	TI	TEMP. INDICATE
RELEASE/ VACUUM VALVE	TSH	TEMP. SWITCH HIGH
ALYZER SWITCH HIGH	TSL	TEMP. SWITCH LOW
ALYZER SWITCH LOW	VI	VACUUM INDICATOR
ALYZER TRANSMITTER	VT	VACUUM TRANSMITTER
OW ELEMENT	YA	STATUS ALARM
OW INDICATOR	YAR	STATUS ALARM RUN
ND SWITCH	YAS	STATUS ALARM STOP
TEL ALARM HIGH/HIGH	YIC	STATUS INDICATE CLOSE
TEL SWITCH HIGH	YIO	STATUS INDICATE OPEN
TEL SWITCH HIGH/HIGH	YIR	STATUS INDICATE RUN
TEL SWITCH LOW/LOW	YIS	STATUS INDICATE STOP
TEL ALARM LOW/LOW	YSR	STATUS SWITCH RUN
TEL SWITCH LOW	ZA	POSITION ALARM
TEL SWITCH	ZAC	POSITION ALARM CLOSE
TEL TRANSMITTER	ZAO	POSITION ALARM OPEN
TORIZED VALVE	ZIC	POSITION INDICATE CLOSE
STURE SENSOR	ZIO	POSITION INDICATE OPEN
INDICATOR/TRANSMITTER	ZSC	POSITION SWITCH CLOSE



# POWER GENERATION ENGINEERING RICHMOND, VIRGINIA

# MECHANICAL P&ID

# RETROFIT – SLUDGE SEDIMENTATION BASINS CLOVER POWER STATION



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## Appendix B: Flood Insurance Rate Map

## NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The **community map repository** should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations** (BFEs) and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

**Coastal Base Flood Elevations** shown on this map apply only landward of 0.0 foot North American Vertical Datum of 1988 (NAVD 88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations tables in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations tables should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway maps and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures**. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Virginia State Plane South zone. The **horizontal datum** was NAD 83, GRS80 spheroid. Differences in datum, spheroid, projection or State Plane zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988. These flood elevations must be compared to structure and ground elevations referenced to the same **vertical datum**. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <http://www.ngs.noaa.gov> or contact the National Geodetic Survey at the following address:

NGS Information Services  
NOAA, NNGS12  
National Geodetic Survey  
SSMC-3, #9202  
1315 East-West Highway  
Silver Spring, Maryland 20910-3282  
(301) 713-3242

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242, or visit its website at <http://www.ngs.noaa.gov>.

**Base map** information shown on this FIRM was provided in digital format by the Commonwealth of Virginia through the Virginia Geographic Network Division of its Department of Technology Planning (VGIN). These data were produced at scales of 1:2,400 and 1:4,800 from one-foot and two-foot resolution digital orthoimagery flown in Spring 2002.

This map reflects more detailed and up-to-date **stream channel configurations** than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways have been transferred from prior panels and may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodways Data tables in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map.

**Corporate limits** shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels, community map repository addresses, and a listing of communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact the **FEMA Map Service Center** at 1-800-358-9616 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study report, and/or digital versions of this map. The FEMA Map Service Center may also be reached by Fax at 1-800-358-9620 and its website at <http://msc.fema.gov>.

If you have questions about this map or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA MAP (1-877-336-2627) or visit the FEMA website at <http://www.fema.gov/business/nfip>.



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## Appendix C: Storm Water Calculations

- Storm Water Run-On Estimate
- Pumping Time Estimate



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## **Storm Water Run-On Estimate**

PROJECT / LOCATION: Clover Power Station - Clover, Virginia		PROJECT / PROPOSAL NO.	
SUBJECT: Storm Water Capacity of North and South Basins		430492.0000	
PREPARED BY: K. Thelen	DATE: 10/7/2021	FINAL	<input type="checkbox"/>
CHECKED BY: J. Hotstream	DATE: 10/8/2021	REVISION	<input type="checkbox"/>

Purpose: Determine the minimum freeboard necessary to control inflow from a 24-hour, 100-year storm event

Methodology:

- 1.) Determine the volume storm water runoff volume that flows into the basins from the 100 year, 24 hour storm event

$$V_R = \text{Volume of Runoff}$$

$$\text{Area} = 5.78 \text{ ac}$$

Rainfall

$$\text{Rate} = 8.01 \text{ in} \quad \text{Design storm data from NOAA, refer to attached sheets}$$

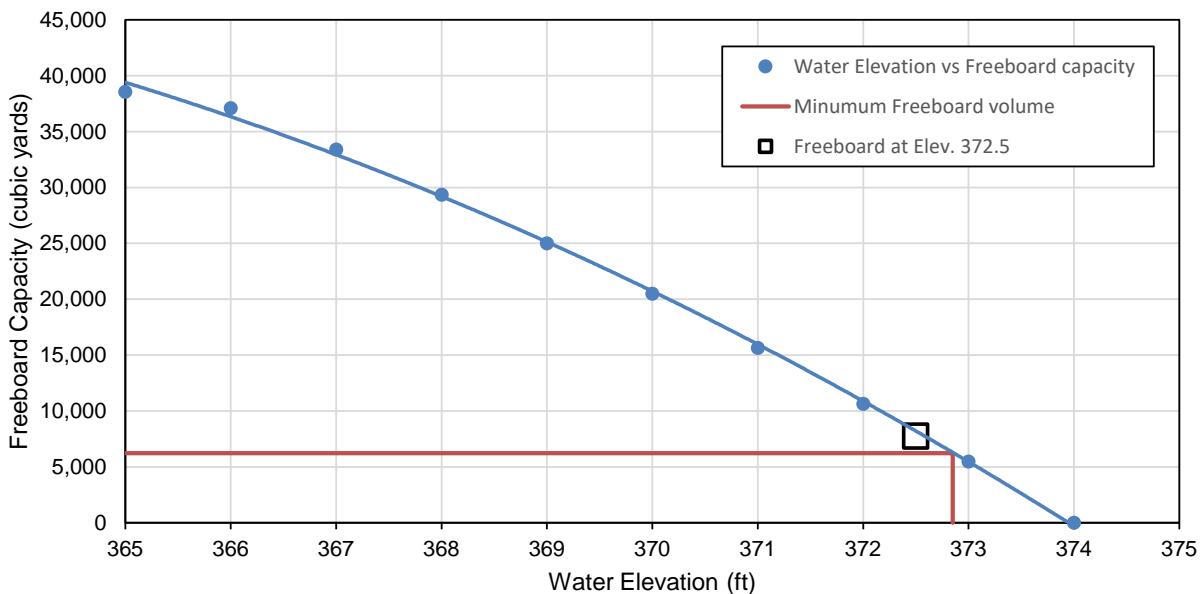
$$V_R = \text{Area} * \text{Rainfall Rate}$$

$$V_R = 6,224 \text{ cy}$$

PROJECT / LOCATION: Clover Power Station - Clover, Virginia		PROJECT / PROPOSAL NO.
SUBJECT: Storm Water Capacity of North and South Basins		430492.0000
PREPARED BY: K. Thelen	DATE: 10/7/2021	FINAL <input type="checkbox"/>
CHECKED BY: J. Hotstream	DATE: 10/8/2021	REVISION <input type="checkbox"/>

- 2.) Find the minimum freeboard elevation which will allow sufficient capacity to control inflow from the 100-year, 24-hour storm event  
 2a) Plot Freeboard Storage vs Freeboard Elevation  
 \*plot developed from stage-storage data, refer to attached table

Water Elevation vs Freeboard Capacity



Find minimum Freeboard Elevation such that SFB > VR

$$E_{FB, \min} = 372.85 \text{ ft}$$

- 3.) Choose a conservative Freeboard Elevation, then compare to VR

$$E_{FB, \text{cons}} = 372.5 \text{ ft}$$

- If freeboard volume ( $S_{FB}$ ) >  $V_R$ , then sufficient freeboard is provided

$$\begin{aligned} S_{FB} &= 7,749 \text{ cy at Elevation 372.5 feet} \\ V_R &= 6,224 \text{ cy} \\ S_{FB} &> V_R \end{aligned}$$

Conclusion: Because the  $S_{FB} > V_R$ , the 1.5 feet of freeboard is capable of containing the runoff volume of the 100-year, 24-hour storm event



PROJECT / LOCATION: Clover Power Station - Clover, Virginia		PROJECT / PROPOSAL NO.
SUBJECT: Storm Water Capacity of North and South Basins		430492.0000
PREPARED BY: K. Thelen	DATE: 10/7/2021	FINAL <input type="checkbox"/>
CHECKED BY: J. Hotstream	DATE: 10/8/2021	REVISION <input type="checkbox"/>

## ATTACHMENTS

From Drawing 6607-15348-CWSG-S3107:

STAGE VS STORAGE MATRIX

ELEV.	North Pond Capacity (CY)	North Pond Capacity (CF)	South Pond Capacity (CY)	South Pond Capacity (CF)	Total Pond Capacity (CY)	Total Pond Capacity (CF)	COMBINED POND CAPACITY (AC FT)	CAPACITY ABOVE TO CREST (AC FT)	CAPACITY ABOVE TO CREST (CY)
365	71	1,924	72	1,937	143	3,861	0.1	23.9	38,561
366	809	21,848	806	21,769	1,615	43,617	1.0	23.0	37,089
367	2,635	71,145	2,613	70,546	5,248	141,691	3.3	20.7	33,457
368	4,700	126,904	4,652	125,617	9,353	252,521	5.8	18.2	29,352
369	6,877	185,666	6,803	183,678	13,679	369,344	8.5	15.5	25,025
370	9,166	247,477	9,066	244,769	18,231	492,246	11.3	12.7	20,473
371	11,570	312,381	11,442	308,930	23,012	621,311	14.3	9.7	15,693
372	14,090	380,420	13,933	376,200	28,023	756,620	17.4	6.6	10,681
373	16,725	451,579	16,539	446,560	33,264	898,138	20.6	3.4	5,440
374	19,461	525,435	19,244	519,583	38,704	1,045,018	24.0	0.0	0



**NOAA Atlas 14, Volume 2, Version 3**  
**Location name: Randolph, Virginia, USA\***  
**Latitude: 36.8698°, Longitude: -78.7018°**  
**Elevation: 372.82 ft\*\***

\* source: ESRI Maps

\*\* source: USGS



### POINT PRECIPITATION FREQUENCY ESTIMATES

G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M. Yekta, and D. Riley

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aerials](#)

### PF tabular

Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	0.364 (0.324-0.408)	0.430 (0.384-0.482)	0.504 (0.449-0.564)	0.564 (0.502-0.629)	0.632 (0.560-0.703)	0.681 (0.600-0.756)	0.727 (0.639-0.808)	0.767 (0.670-0.854)	0.815 (0.708-0.908)	0.852 (0.734-0.950)
10-min	0.582 (0.518-0.652)	0.688 (0.614-0.771)	0.808 (0.720-0.903)	0.903 (0.803-1.01)	1.01 (0.892-1.12)	1.08 (0.956-1.21)	1.16 (1.01-1.28)	1.22 (1.06-1.35)	1.29 (1.12-1.44)	1.34 (1.16-1.50)
15-min	0.727 (0.648-0.815)	0.865 (0.771-0.969)	1.02 (0.910-1.14)	1.14 (1.02-1.27)	1.28 (1.13-1.42)	1.37 (1.21-1.53)	1.46 (1.28-1.62)	1.54 (1.34-1.71)	1.62 (1.41-1.81)	1.68 (1.45-1.88)
30-min	0.997 (0.888-1.12)	1.20 (1.07-1.34)	1.45 (1.29-1.62)	1.65 (1.47-1.85)	1.89 (1.68-2.10)	2.07 (1.82-2.30)	2.24 (1.97-2.49)	2.39 (2.09-2.66)	2.58 (2.24-2.88)	2.73 (2.35-3.04)
60-min	1.24 (1.11-1.39)	1.50 (1.34-1.68)	1.86 (1.66-2.08)	2.15 (1.92-2.40)	2.52 (2.23-2.80)	2.80 (2.47-3.11)	3.08 (2.71-3.42)	3.35 (2.93-3.73)	3.70 (3.22-4.13)	3.98 (3.43-4.44)
2-hr	1.47 (1.31-1.66)	1.77 (1.57-1.99)	2.21 (1.96-2.49)	2.59 (2.29-2.90)	3.07 (2.70-3.43)	3.47 (3.03-3.86)	3.87 (3.35-4.30)	4.27 (3.68-4.75)	4.82 (4.11-5.36)	5.25 (4.45-5.85)
3-hr	1.57 (1.40-1.77)	1.90 (1.69-2.14)	2.37 (2.10-2.67)	2.77 (2.45-3.11)	3.29 (2.90-3.69)	3.72 (3.25-4.16)	4.15 (3.61-4.63)	4.58 (3.96-5.11)	5.17 (4.42-5.77)	5.64 (4.78-6.30)
6-hr	1.92 (1.70-2.17)	2.31 (2.05-2.61)	2.88 (2.55-3.26)	3.39 (2.99-3.82)	4.06 (3.56-4.57)	4.64 (4.04-5.21)	5.23 (4.52-5.87)	5.86 (5.01-6.55)	6.73 (5.68-7.50)	7.45 (6.21-8.31)
12-hr	2.30 (2.07-2.60)	2.77 (2.49-3.13)	3.47 (3.11-3.91)	4.12 (3.67-4.63)	5.00 (4.42-5.59)	5.77 (5.06-6.42)	6.59 (5.72-7.34)	7.46 (6.41-8.26)	8.73 (7.37-9.64)	9.82 (8.16-10.9)
24-hr	2.68 (2.46-2.95)	3.25 (2.98-3.58)	4.15 (3.79-4.57)	4.90 (4.47-5.39)	6.02 (5.44-6.59)	6.97 (6.27-7.63)	8.01 (7.15-8.75)	9.15 (8.10-9.99)	10.8 (9.46-11.8)	12.3 (10.6-13.4)
2-day	3.15 (2.90-3.45)	3.82 (3.52-4.18)	4.84 (4.45-5.29)	5.68 (5.21-6.20)	6.89 (6.29-7.52)	7.91 (7.18-8.63)	9.00 (8.11-9.82)	10.2 (9.10-11.1)	11.9 (10.5-13.0)	13.3 (11.6-14.6)
3-day	3.33 (3.07-3.65)	4.03 (3.72-4.42)	5.11 (4.70-5.59)	6.00 (5.50-6.56)	7.28 (6.64-7.95)	8.34 (7.57-9.10)	9.49 (8.55-10.4)	10.7 (9.59-11.7)	12.5 (11.1-13.7)	14.0 (12.2-15.3)
4-day	3.52 (3.23-3.85)	4.25 (3.91-4.66)	5.39 (4.95-5.89)	6.32 (5.79-6.91)	7.66 (6.99-8.37)	8.78 (7.97-9.57)	9.98 (9.00-10.9)	11.3 (10.1-12.3)	13.1 (11.6-14.4)	14.7 (12.9-16.1)
7-day	4.05 (3.73-4.42)	4.87 (4.49-5.32)	6.07 (5.59-6.62)	7.06 (6.48-7.69)	8.47 (7.73-9.22)	9.64 (8.76-10.5)	10.9 (9.82-11.8)	12.2 (10.9-13.3)	14.1 (12.5-15.4)	15.7 (13.7-17.1)
10-day	4.60 (4.26-5.00)	5.51 (5.10-5.99)	6.80 (6.28-7.38)	7.83 (7.23-8.50)	9.30 (8.55-10.1)	10.5 (9.60-11.4)	11.7 (10.7-12.7)	13.1 (11.8-14.1)	14.9 (13.3-16.2)	16.4 (14.6-17.8)
20-day	6.23 (5.81-6.71)	7.42 (6.92-7.98)	8.96 (8.34-9.63)	10.2 (9.44-10.9)	11.8 (10.9-12.7)	13.1 (12.1-14.1)	14.4 (13.2-15.5)	15.7 (14.4-16.9)	17.5 (15.9-18.9)	18.9 (17.1-20.4)
30-day	7.70 (7.23-8.20)	9.12 (8.57-9.70)	10.8 (10.1-11.5)	12.0 (11.3-12.8)	13.7 (12.8-14.5)	14.9 (13.9-15.8)	16.1 (15.0-17.1)	17.3 (16.1-18.4)	18.9 (17.4-20.1)	20.0 (18.4-21.4)
45-day	9.71 (9.16-10.3)	11.5 (10.8-12.1)	13.4 (12.6-14.2)	14.8 (13.9-15.7)	16.7 (15.6-17.6)	18.0 (16.9-19.1)	19.3 (18.1-20.5)	20.6 (19.2-21.9)	22.2 (20.6-23.6)	23.4 (21.6-24.9)
60-day	11.6 (11.0-12.2)	13.6 (12.9-14.4)	15.7 (14.8-16.6)	17.3 (16.3-18.2)	19.3 (18.2-20.3)	20.7 (19.5-21.9)	22.1 (20.8-23.4)	23.4 (21.9-24.8)	25.1 (23.4-26.6)	26.2 (24.4-27.9)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

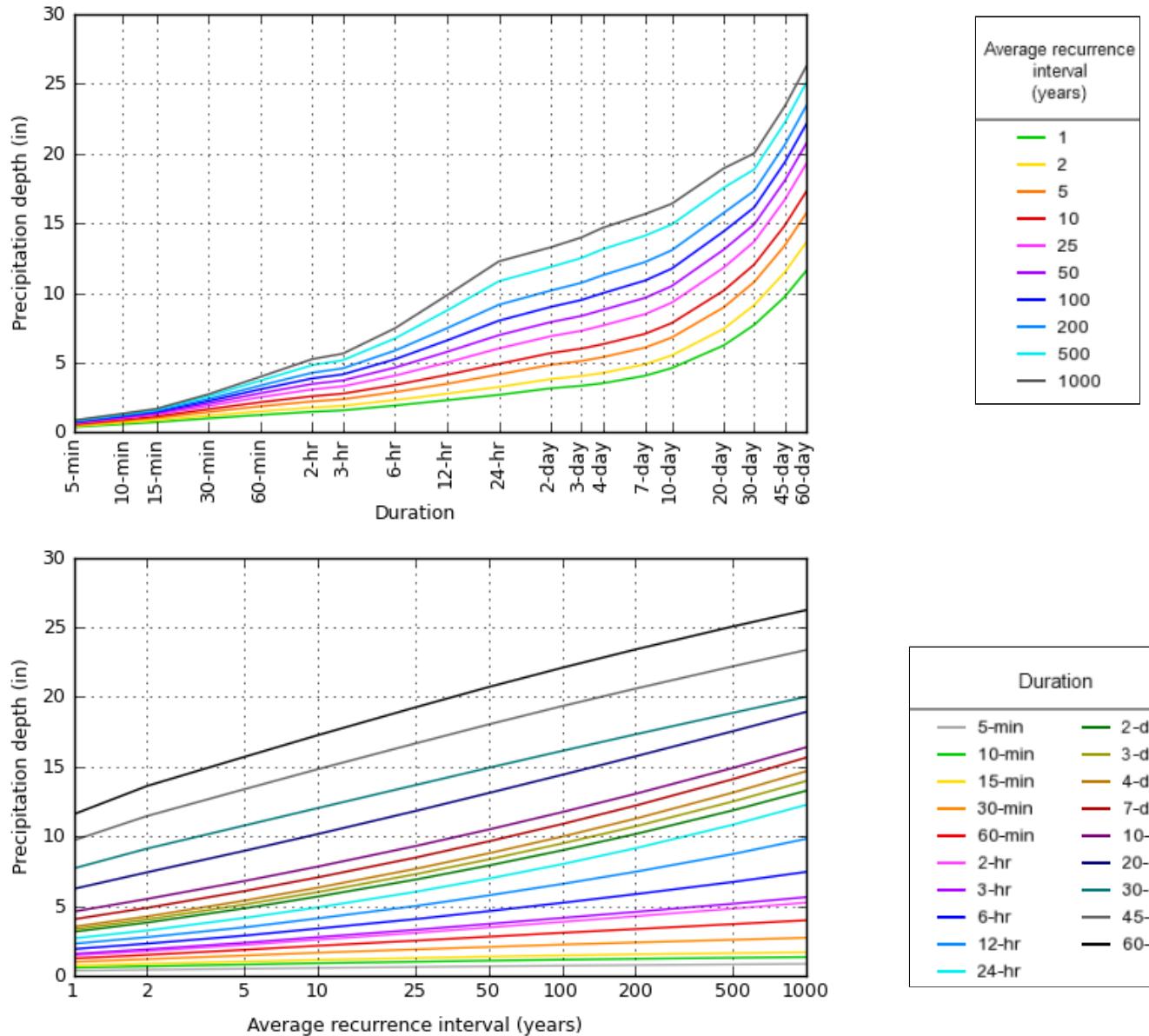
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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### PF graphical

PDS-based depth-duration-frequency (DDF) curves  
Latitude: 36.8698°, Longitude: -78.7018°



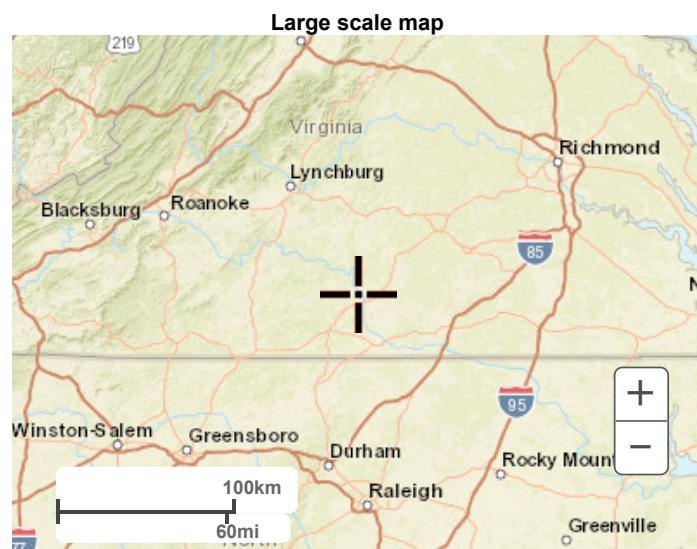
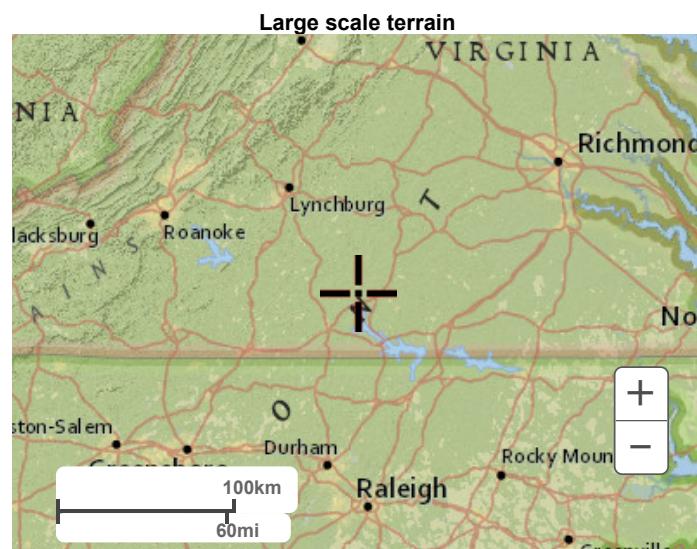
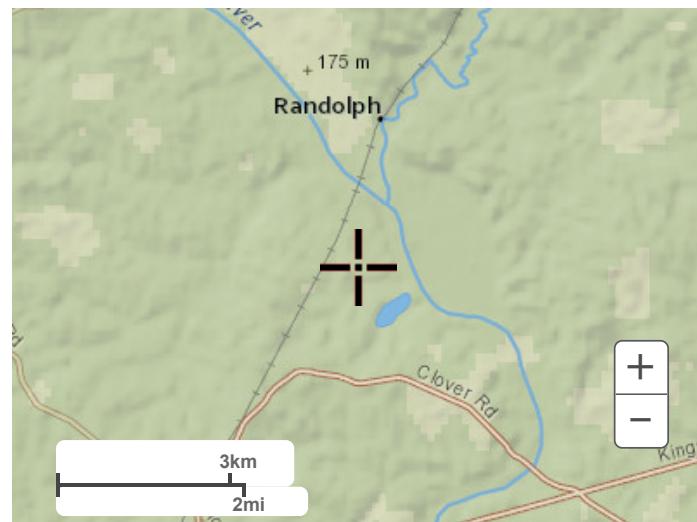
NOAA Atlas 14, Volume 2, Version 3

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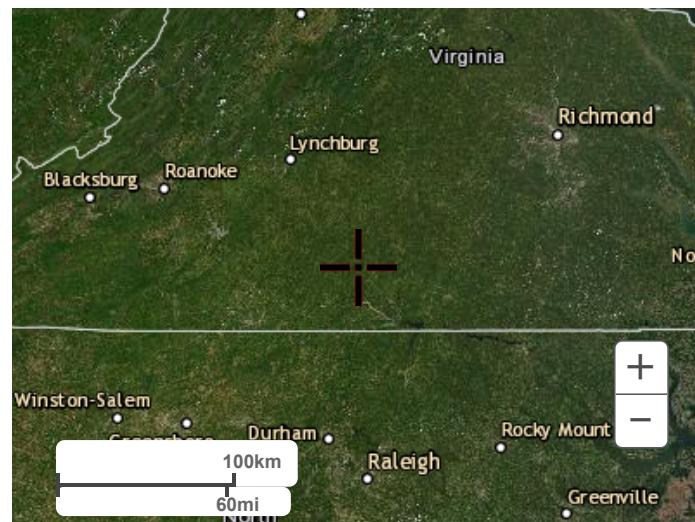
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## Maps & aerials

[Small scale terrain](#)



Large scale aerial

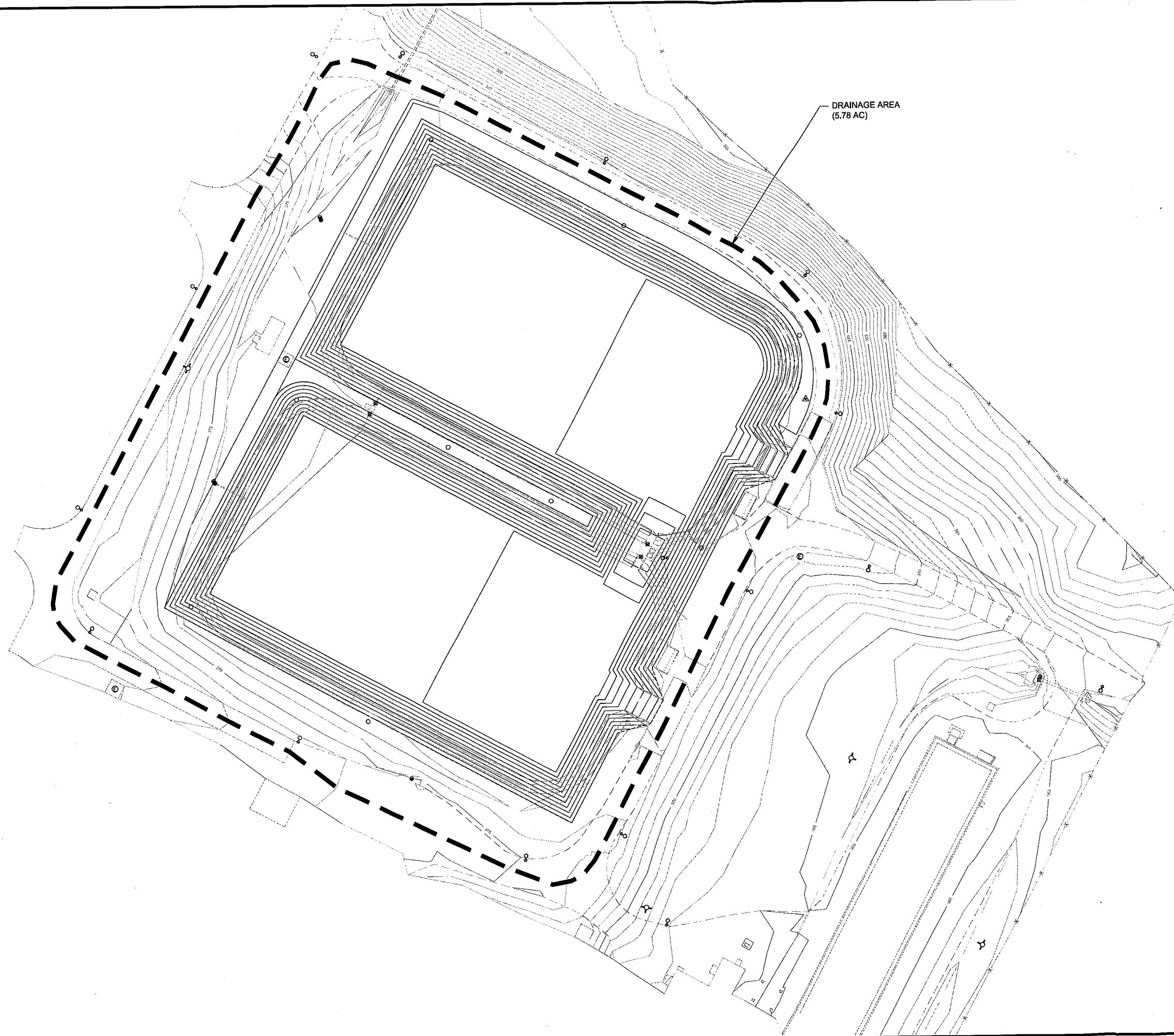


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Silver Spring, MD 20910  
Questions?: [HDSC.Questions@noaa.gov](mailto:HDSC.Questions@noaa.gov)

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NO.	BY	DATE	REVISION	APPD.
PROJECT: DOMINION RESOURCES SERVICES, INC. CLOVER POWER STATION				
RETROFIT - EMERGENCY SLUDGE STORAGE PONDS CLOVER, VIRGINIA				
TITLE: WORKING COPY				
DRAWN BY:	E. OLSON	PROJ. NO.:	232002.0000.0000 00004	
CHECKED BY:	—	APPROVED BY:	F-01	
APPROVED BY:	—	DATE:	NOVEMBER 2015	
30 Patewood Drive Patewood Plaza One, Suite 300 Greenville, SC 29615 Phone: 864.281.0030				
FILE NO.: F-01_Drainage Areas and Tc.dwg				

06



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## Pumping Time Estimate



PROJECT / LOCATION: Clover Power Station - Clover, Virginia		PROJECT / PROPOSAL NO.
SUBJECT: Estimated Pump Down Time		430492.0000
PREPARED BY: K. Thelen	DATE: 7/29/21	FINAL <input type="checkbox"/>
CHECKED BY: J. Hotstream	DATE: 8/22/21	REVISION <input type="checkbox"/>

Purpose: Determine the amount of time needed for a Lawrence VPL3200 Pump to remove the storm water collected during the 100-year, 24-hour storm event to design operation elevation (ELE 372)

Methodology:

- 1.) Use the volume of runoff collected in the basins for the 100-year, 24-hour storm (V R) from the Freeboard Volume Calculation

- Volume of Runoff

$$V_R = 6,224 \text{ cy}$$

- 2.) Use pump capacity rating to determine amount of time to lower the water level in both basins to ELE 372

- Assume only one pump is operational for both ponds

$$\text{Pump Rate} = 410 \text{ gallons per minute (gpm)}$$

$$\begin{aligned} V_R &= 6,224 \text{ cy} \\ V_R &= 1,257,086 \text{ gal} \end{aligned}$$

$$\text{Time} = \frac{V_R}{\text{Pump Rate}}$$

$$\begin{aligned} \text{Time} &= 3,066 \text{ min} \\ &= 51.1 \text{ hr} \\ &= 2.1 \text{ days} \end{aligned}$$

Conclusion: It will take approximately 2 days to pump out the storm water to reestablish freeboard after the 100-year, 24-hour storm event.

This calculation assumes that only one pump will be in operation to remove stormwater.