

INFLOW DESIGN FLOOD CONTROL SYSTEM PLAN

Possum Point Power Station CCR Surface Impoundments: Ponds ABC



Submitted To: Possum Point Power Station

19000 Possum Point Road Dumfries, VA 22026

Submitted By: Golder Associates Inc.

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April 2018

Project No. 16-62150

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1.0 CERTIFICATION

This Inflow Design Flood Control System Plan for the Possum Point Power Station's Ponds ABC was prepared by Golder Associates Inc. (Golder). The document and Certification/Statement of Professional Opinion are based on and limited to information that Golder has relied on from Dominion and others, but not independently verified, as well as work products produced by Golder.

On the basis of and subject to the foregoing, it is my professional opinion as a Professional Engineer licensed in the Commonwealth of Virginia that this document has been prepared in accordance with good and accepted engineering practices as exercised by other engineers practicing in the same discipline(s), under similar circumstances, at the same time, and in the same locale. It is my professional opinion that the document was prepared consistent with the requirements in §257.73(c) of the United States Environmental Protection Agency's "Standards for the Disposal of Coal Combustion Residuals in Landfills and Surface Impoundments," published in the Federal Register on April 17, 2015, with an effective date of October 19, 2015 [40 CFR §257.73(c)], as well as with the requirements in §257.100 resulting from the EPA's "Hazardous and Solid Waste Management System: Disposal of Coal Combustion Residuals From Electric Utilities; Extension of Compliance Deadlines for Certain Inactive Surface Impoundments; Response to Partial Vacatur" published in the Federal Register on August 5, 2016 with an effective date of October 4, 2016 (40 CFR §257.100).

The use of the word "certification" and/or "certify" in this document shall be interpreted and construed as a Statement of Professional Opinion, and is not and shall not be interpreted or construed as a guarantee, warranty, or legal opinion.

Daniel McGrath	Associat	e and Senior Cons	ultant
Print Name	Title		
Daniel M'Krath		4/13/18	
Signature	Date		
	Daniel M' Math 3		
	Lic. No. 040703		
	4/13/18 CSSIONAL ENGINE		
	SONAL PARTIES		



2.0 INTRODUCTION

This Inflow Design Flood Control System (FCS) Plan was prepared for the Possum Point Power Station's (Station) inactive Coal Combustion Residuals (CCR) surface impoundments, Ponds ABC. This FCS Plan was prepared in accordance with 40 CFR Part §257, Subpart D and is consistent with the requirements of 40 CFR §257.82.

Possum Point, owned and operated by Virginia Electric and Power Company d/b/a Dominion Energy Virginia (Dominion), is located in Dumfries, Virginia at 19000 Possum Point Road. The Station includes inactive CCR surface impoundments Ponds ABC as defined by the Disposal of Coal Combustion Residuals from Electric Utilities; Final Rule (40 CFR §257; the CCR rule). In anticipation of closure, Ponds ABC are being excavated and the material placed in Pond D. This FCS Plan has been developed based on the existing Ponds ABC topography as of April 28, 2017.

3.0 INFLOW DESIGN FLOOD CONTROL SYSTEM PLAN

3.1 Hazard Potential Classification

As indicated in Golder's *Hazard Potential Classification Assessment*, Ponds ABC is assigned a "Significant" hazard potential rating per 40 CFR §257.73.

3.2 Inflow Design Flood

According to 40 CFR §257.82(a)(3)(ii), a hazard potential rating of Significant requires an evaluation of the ponds and appurtenances to handle a 1000-year storm event. Per the NOAA Atlas-14, provided in Appendix A, the 1000-year event rainfall total for the 24-hour duration is 13.6 inches.

3.3 Inflow and Outflow Control

Inflow to the ponds is primarily stormwater runoff from within the units (14.0 ac) and the adjacent area south of Possum Point Road (18.2 ac); however, approximately 8.4 acres from north of Possum Point Road also drain into the pond. The total drainage area to the ponds is approximately 40.6 acres. The majority of stormwater arrives through overland flow. Other than maintaining pre-established runoff control measures, there are no inflow control measures proposed.

The ponds' primary outlet for stormwater is a 4-ft by 4-ft square riser, fitted with stoplogs, that discharges through a 30-inch reinforced concrete pipe (RCP) into the adjacent Quantico Creek. This demonstration assumes that the permanent pool is maintained below the stoplog crest. The stage-storage curve for Ponds ABC was developed using the April 28, 2017 topography, and shows that Ponds ABC has approximately 117.5 acre-feet of available water storage volume at the embankment crest (approximately el. 20.0 ft).



The ponds' stormwater system was modeled in the U.S. Army Corps of Engineers Hydrologic Engineering Center's Hydraulic Modeling System (HEC-HMS), and the analysis is included in Appendix B. The analysis was conducted using the 24-hour, 1,000-year event, which was modeled as 13.6 inches of rain. Based on this analysis, the ponds' inflow design flood control system is capable of adequately managing the inflow from the 1,000-year event without overtopping the embankment.

The following table summarizes the results of the HEC-HMS analysis for the 1,000-year storm event.

Table 1: HEC-HMS Output

Q _{in} (CFS)	Max Hw (Ft EI*)	Primary Q _{out} (CFS)
301.2	10.4	0.0

^{*} Top of berm elevation = el. 20.0 ft

4.0 CONCLUSIONS

Through work performed by Golder, both field inspection and document review, it is our opinion that the Ponds ABC inflow design flood control system has sufficient capacity for the 1000-year storm event, as required by 40 CFR §257.82.







NOAA Atlas 14, Volume 2, Version 3 Location name: Dumfries, Virginia, USA* Latitude: 38.5466°, Longitude: -77.2872° Elevation: 15.59 ft**

* source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M.Yekta, and D. Riley

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

PF tabular

PDS	S-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹										
Duration				Averaç	ge recurrenc	e interval (y	/ears)				
Duration	1	2	5	10	25	50	100	200	500	1000	
5-min	0.356 (0.322-0.393)	0.427 (0.387-0.471)	0.508 (0.459-0.560)	0.567 (0.511-0.625)	0.642 (0.575-0.708)	0.698 (0.623-0.770)	0.754 (0.669-0.833)	0.808 (0.712-0.895)	0.878 (0.765-0.977)	0.933 (0.807-1.04)	
10-min	0.569 (0.515-0.628)	0.683 (0.619-0.753)	0.813 (0.736-0.897)	0.907 (0.818-1.00)	1.02 (0.917-1.13)	1.11 (0.992-1.23)	1.20 (1.06-1.32)	1.28 (1.13-1.42)	1.39 (1.21-1.55)	1.47 (1.27-1.64)	
15-min	0.711 (0.644-0.784)	0.859 (0.778-0.946)	1.03 (0.931-1.14)	1.15 (1.03-1.26)	1.30 (1.16-1.43)	1.41 (1.26-1.55)	1.51 (1.34-1.67)	1.62 (1.42-1.79)	1.75 (1.52-1.95)	1.84 (1.59-2.06)	
30-min	0.975 (0.882-1.08)	1.19 (1.07-1.31)	1.46 (1.32-1.61)	1.66 (1.50-1.83)	1.92 (1.72-2.12)	2.12 (1.89-2.34)	2.32 (2.06-2.56)	2.52 (2.22-2.79)	2.78 (2.42-3.10)	2.99 (2.58-3.34)	
60-min	1.22 (1.10-1.34)	1.49 (1.35-1.64)	1.87 (1.70-2.07)	2.17 (1.95-2.39)	2.56 (2.29-2.82)	2.87 (2.56-3.17)	3.20 (2.83-3.53)	3.53 (3.11-3.91)	3.99 (3.48-4.44)	4.36 (3.77-4.87)	
2-hr	1.42 (1.28-1.57)	1.73 (1.56-1.91)	2.19 (1.98-2.42)	2.56 (2.29-2.82)	3.06 (2.74-3.39)	3.48 (3.09-3.85)	3.92 (3.45-4.33)	4.38 (3.83-4.85)	5.03 (4.35-5.60)	5.56 (4.76-6.22)	
3-hr	1.53 (1.38-1.71)	1.86 (1.67-2.08)	2.36 (2.12-2.64)	2.76 (2.47-3.08)	3.33 (2.95-3.70)	3.79 (3.34-4.22)	4.29 (3.75-4.77)	4.81 (4.17-5.37)	5.57 (4.76-6.24)	6.19 (5.23-6.96)	
6-hr	1.88 (1.70-2.11)	2.28 (2.05-2.56)	2.88 (2.59-3.23)	3.38 (3.01-3.77)	4.10 (3.63-4.58)	4.71 (4.14-5.26)	5.38 (4.68-6.01)	6.10 (5.25-6.83)	7.15 (6.06-8.05)	8.04 (6.72-9.09)	
12-hr	2.28 (2.04-2.57)	2.76 (2.47-3.10)	3.50 (3.12-3.94)	4.13 (3.67-4.64)	5.09 (4.48-5.71)	5.92 (5.16-6.64)	6.85 (5.90-7.69)	7.88 (6.69-8.85)	9.44 (7.86-10.7)	10.8 (8.84-12.2)	
24-hr	2.57 (2.33-2.88)	3.12 (2.83-3.49)	4.03 (3.65-4.51)	4.83 (4.36-5.39)	6.05 (5.41-6.72)	7.12 (6.33-7.88)	8.33 (7.35-9.19)	9.70 (8.48-10.7)	11.8 (10.2-12.9)	13.6 (11.6-14.9)	
2-day	2.98 (2.70-3.32)	3.62 (3.28-4.03)	4.67 (4.23-5.20)	5.58 (5.03-6.20)	6.95 (6.22-7.68)	8.14 (7.25-8.98)	9.47 (8.36-10.4)	11.0 (9.59-12.1)	13.2 (11.4-14.5)	15.2 (12.9-16.7)	
3-day	3.16 (2.87-3.52)	3.84 (3.48-4.27)	4.94 (4.47-5.49)	5.88 (5.31-6.53)	7.30 (6.55-8.07)	8.54 (7.62-9.41)	9.91 (8.76-10.9)	11.4 (10.0-12.6)	13.7 (11.9-15.1)	15.7 (13.5-17.3)	
4-day	3.35 (3.04-3.72)	4.06 (3.68-4.51)	5.21 (4.72-5.78)	6.19 (5.60-6.86)	7.66 (6.88-8.46)	8.93 (7.98-9.85)	10.3 (9.17-11.4)	11.9 (10.5-13.1)	14.3 (12.4-15.7)	16.3 (14.0-17.9)	
7-day	3.89 (3.56-4.27)	4.69 (4.30-5.16)	5.94 (5.43-6.52)	6.99 (6.38-7.67)	8.57 (7.78-9.38)	9.92 (8.95-10.8)	11.4 (10.2-12.4)	13.0 (11.6-14.2)	15.5 (13.6-16.8)	17.5 (15.2-19.1)	
10-day	4.46 (4.10-4.87)	5.35 (4.92-5.85)	6.68 (6.14-7.29)	7.78 (7.13-8.48)	9.37 (8.56-10.2)	10.7 (9.74-11.6)	12.1 (11.0-13.2)	13.7 (12.3-14.9)	15.9 (14.2-17.3)	17.8 (15.7-19.3)	
20-day	6.00 (5.58-6.49)	7.15 (6.64-7.72)	8.64 (8.02-9.32)	9.85 (9.14-10.6)	11.5 (10.7-12.4)	12.9 (11.9-13.9)	14.3 (13.1-15.4)	15.8 (14.4-17.0)	17.8 (16.2-19.2)	19.5 (17.5-21.0)	
30-day	7.37 (6.88-7.91)	8.72 (8.15-9.36)	10.4 (9.69-11.1)	11.7 (10.9-12.5)	13.5 (12.6-14.5)	15.0 (13.9-16.0)	16.4 (15.2-17.6)	17.9 (16.5-19.2)	20.0 (18.3-21.4)	21.6 (19.6-23.1)	
45-day	9.27 (8.70-9.84)	10.9 (10.3-11.6)	12.8 (12.0-13.6)	14.2 (13.4-15.1)	16.1 (15.1-17.1)	17.5 (16.4-18.6)	18.9 (17.7-20.1)	20.3 (18.9-21.6)	22.1 (20.5-23.5)	23.4 (21.6-24.9)	
60-day	11.0 (10.4-11.6)	12.9 (12.2-13.7)	15.0 (14.1-15.8)	16.5 (15.5-17.4)	18.4 (17.4-19.5)	19.9 (18.7-21.0)	21.2 (19.9-22.5)	22.5 (21.1-23.9)	24.2 (22.6-25.6)	25.4 (23.6-26.9)	

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

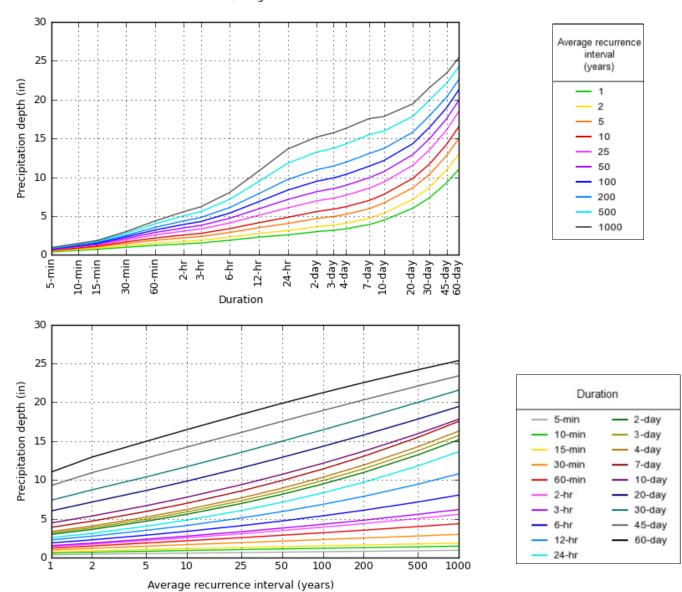
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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PF graphical

PDS-based depth-duration-frequency (DDF) curves Latitude: 38.5466°, Longitude: -77.2872°



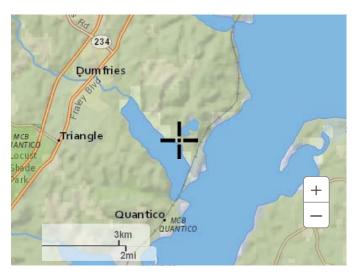
NOAA Atlas 14, Volume 2, Version 3

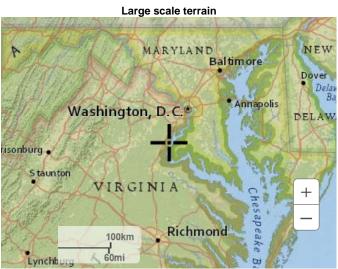
Created (GMT): Thu Jan 25 21:42:03 2018

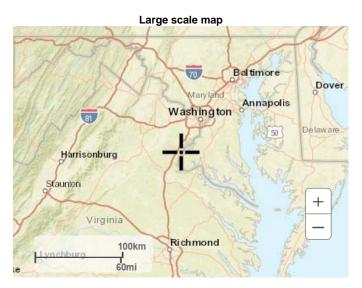
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Maps & aerials

Small scale terrain







Large scale aerial



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US Department of Commerce National Oceanic and Atmospheric Administration
National Weather Service National Water Center
1325 East West Highway
Silver Spring, MD 20910
Questions?: HDSC.Questions@noaa.gov

Disclaimer

APPENDIX B

Hydraulic Modeling Analysis



CALCULATIONS

Date:February 7, 2018Made by:KALProject No.:16-62150Checked by:SDRM

Subject: PPPS Ponds ABC Inflow Design Flood Reviewed by: DPM

Analysis

Project: POSSUM POINT POWER STATION PONDS ABC – EXISTING CONDITION

The purpose of this evaluation is to determine the hydraulic performance of the existing Ponds ABC CCR impoundment at the Possum Point Power Station (PPPS) during the 1,000-year storm event. This evaluation is in support of the Inflow Design Flood Control System Plan, and is based on a "Significant" hazard potential classification as defined in §257.53 of the *CCR Rule*.

1.0 CALCULATIONS

1.1 Pond Storage Volume

Ponds ABC's storage volume was computed based on the existing condition, as surveyed in April 2017, which is excavated and visually clean of CCR. The maximum available storage in the ponds is approximately 118 acre-feet at elevation 20.0, with overtopping occurring above elevation 20.0. Attachment 1 contains the stage storage rating table used in the HMS model.

1.2 Outlet Design and Capacity

The existing Ponds ABC outfall structure consists of a rectangular riser box fitted with stoplogs to adjust the pond's permanent pool. For this analysis, the ponds were conservatively evaluated with a permanent pool at elevation 0.0 ft (approximately 3.7 ft of water) and no discharge through the riser structure.

1.3 Storm Routing Calculations

Analysis of the Ponds ABC stormwater system was performed using the US Army Corps of Engineers Hydrologic Engineering Center's Hydraulic Modeling System (HEC-HMS) software package (ref #1). The direct drainage area to the pond is 40.6 acres. The predominant soil types in the area are Hydrologic Soil Group (HSG) B soils.

Per §257.82(a)(3)(ii), the impoundments are required to adequately manage flow resulting from the 1,000-Yr storm event. The 24-hour, 1,000-Yr storm event precipitation amount was obtained from the Precipitation Frequency Data Server (PFDS, ref #2) for Dumfires, Virginia, as 13.6 inches.

Figure 1 illustrates the connectivity of the stormwater elements and the data inputs as modeled in HEC-HMS.



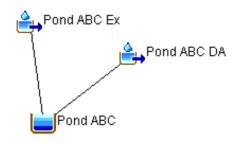


Figure 1 - PPPS Ponds ABC HEC-HMS Model

The following table summarizes the results of the HEC-HMS analysis for the 1,000-Yr storm event.

Table 1: PP ABC HEC-HMS Output

Q _{in} (CFS)	Max Hw (Ft EI*)	Primary Q _{out} (CFS)
301.2	10.4	0.0

^{*} Top of berm elevation = el. 20.0 ft

2.0 CONCLUSIONS

Based on the calculations presented herein, Ponds ABC can pass the 1,000-Yr event without overtopping.

3.0 REFERENCES

- 1) U.S. Army Corps of Engineers Hydrologic Engineering Center Hydrologic Modeling System (HEC-HMS) release 4.2.1
- 2) Precipitation Frequency Data Server (NOAA Atlas 14) https://hdsc.nws.noaa.gov/hdsc/pfds/

4.0 ATTACHMENTS

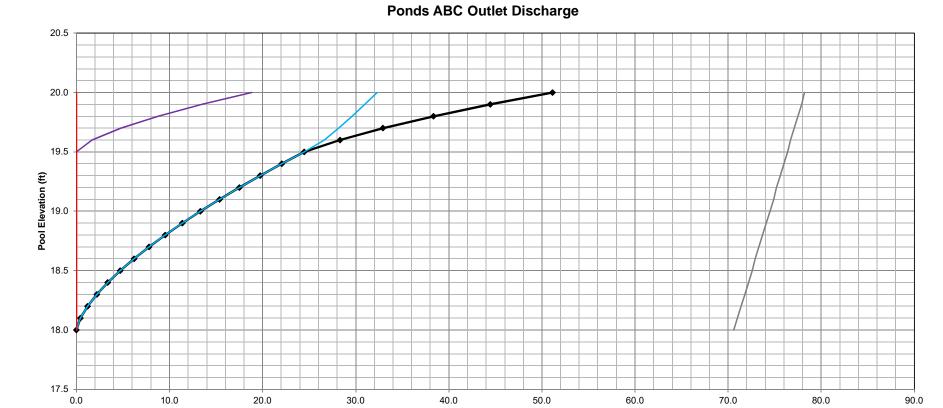
- 1) Stage-Storage Table
- 2) Outlet Discharge
- 3) HEC-HMS



Ponds ABC Stage-Storage Table

Elevation	Area	a	Volu	me	Cumu	lative Volume		
(ft)	(sqft)	(acres)	(cuft) (CY)		(CY)	(cuft)	(ac-ft)	
20.00	476451.1	10.938	465179.08	17228.85	189550.15	5117854	117.49	
19.00	453997.4	10.422	443364.94	16420.92	172321.29	4652675	106.81	
18.00	432816.8	9.936	424957.17	15739.15	155900.37	4209310	96.63	
17.00	417145.7	9.576	408225.28	15119.45	140161.22	3784353	86.88	
16.00	399369.4	9.168	390036.01	14445.78	125041.76	3376128	77.51	
15.00	380776.5	8.741	371786.75	13769.88	110595.98	2986092	68.55	
14.00	362868.9	8.330	355263.86	13157.92	96826.10	2614305	60.02	
13.00	347712.7	7.982	340816.74	12622.84	83668.18	2259041	51.86	
12.00	333966.9	7.667	307828.51	11401.06	71045.34	1918224	44.04	
11.00	282410.1	6.483	267426.52	9904.69	59644.28	1610396	36.97	
10.00	252717.8	5.802	240154.99	8894.63	49739.60	1342969	30.83	
9.00	227807.6	5.230	214764.61	7954.24	40844.97	1102814	25.32	
8.00	201980.5	4.637	189733.98	7027.18	32890.72	888050	20.39	
7.00	177745.5	4.080	162850.36	6031.49	25863.54	698316	16.03	
6.00	148396.3	3.407	137395.04	5088.71	19832.05	535465	12.29	
5.00	126680.0	2.908	112761.64	4176.36	14743.34	398070	9.14	
4.00	99394.2	2.282	73262.97	2713.44	10566.98	285309	6.55	
3.00	49940.5	1.146	47051.52	1742.65	7853.54	212046	4.87	
2.00	44220.5	1.015	41366.67	1532.10	6110.89	164994	3.79	
1.00	38577.0	0.886	35973.36	1332.35	4578.79	123627	2.84	
0.00	33431.1	0.767	30512.84	1130.11	3246.45	87654	2.01	
-1.00	27684.9	0.636	25183.87	932.74	2116.34	57141	1.31	
-2.00	22763.1	0.523	20525.54	760.21	1183.60	31957	0.73	
-3.00	18366.5	0.422	11431.79	423.40	423.40	11432	0.26	
-3.70	14377.0	0.330	-	-	-	-	-	

Bas	sin Elevation	S						
Invert	-3.7	ft						
Embankment	20	ft						
1. De	watering Dev	rice	2. P	rincipal Sp	illway			
Туре:	[N	one]	Type:	Red	ct. Weir			
Invert		ft	Crest	18	ft			
Width		in	Width	48	in			
Cd (orifice)	0.6		Cd (orifice)	0.6				
Cw (weir)	3.33		Cw (weir)	3.33				
Orifice Area	0.00	ft2	Orifice Area	6.00	ft2			
Multiple Rows? (Y	or N)	N	Number of Spi	Number of Spillways: 1				
3. Sec	ondary Spill	way	4.	Discharge	Pipe			
Туре:	Rise	r (Box)	Invert	8	ft/ft			
Connect to PS?	Yes		Diameter	30	in			
Crest	19.5	ft	Slope	0.0167	ft/ft	out=3		
Width	48	in	Length	60	ft/ft			
Cd (orifice)	0.6		Material	RCP				
Cw (weir)	3.33		Manning n	0.013				
Riser Area	16.00	ft2						
Number of Spillwa	ıys:	1						
5. Eme	ergency Spill	way						
B. Width	100	ft						
Side Slope	10	:1						
Invert	20	ft						
Top Width	100	ft						



Discharge (cfs)

Total Discharge —— Dewatering Device: [None] —— Principal Spillway: Rect. Weir —— Secondary Spillway: Riser (Box) —— Barrel —— Emergency Spillway

90.0

interval	0.1	Inlet-Controlled Discharge										Outlet	Controlled Di	scharge								
		Davis	tanina Davisas	[Name]			Principal Spillway: Rect. Weir				Secondary Spillway: Riser (Box)							ou On illeure				
Water Elevation		Dewa	tering Device:	[None]			-	<u> </u>	ct. weir	<u> </u>		, , , ,		T	Barrel-		Actual	Emergen	Emergency Spillway		Total	
	Head		Discharge		Controlling	Head		harge	Controlling	Controlling	Head		Discharge		Controlling	Controlled Discharge	Controlling	Discharge	Head	Discharge		Discharge
		Skimmer	Orifice	Weir	Discharge		Orifice	Weir	Condition	Discharge		Orifice	Weir	Condition	Discharge		Condition					
(ft)	(ft)	(cfs)	(cfs)	(cfs)	(cfs)	(ft)	(cfs)	(cfs)		(cfs)	(ft)	(cfs)	(cfs)		(cfs)	(cfs)		(cfs)	(ft)	(cfs)	(ft)	(cfs)
18.00					0.00	0.00		0.00	Weir	0.00					0.00	70.60	Inlet	0.00	0	0.00	21.70	0.00
18.10					0.00	0.10		0.42	Weir	0.42					0.00	71.00	Inlet	0.42	0	0.00	21.80	0.42
18.20					0.00	0.20		1.19	Weir	1.19					0.00	71.40	Inlet	1.19	0	0.00	21.90	1.19
18.30					0.00	0.30		2.19	Weir	2.19					0.00	71.80	Inlet	2.19	0	0.00	22.00	2.19
18.40					0.00	0.40		3.37	Weir	3.37					0.00	72.20	Inlet	3.37	0	0.00	22.10	3.37
18.50					0.00	0.50		4.71	Weir	4.71					0.00	72.60	Inlet	4.71	0	0.00	22.20	4.71
18.60					0.00	0.60		6.19	Weir	6.19					0.00	72.90	Inlet	6.19	0	0.00	22.30	6.19
18.70					0.00	0.70		7.80	Weir	7.80					0.00	73.30	Inlet	7.80	0	0.00	22.40	7.80
18.80					0.00	0.80		9.53	Weir	9.53					0.00	73.70	Inlet	9.53	0	0.00	22.50	9.53
18.90					0.00	0.90		11.37	Weir	11.37					0.00	74.10	Inlet	11.37	0	0.00	22.60	11.37
19.00					0.00	1.00		13.32	Weir	13.32					0.00	74.50	Inlet	13.32	0	0.00	22.70	13.32
19.10					0.00	1.10		15.37	Weir	15.37					0.00	74.90	Inlet	15.37	0	0.00	22.80	15.37
19.20					0.00	1.20		17.51	Weir	17.51					0.00	75.20	Inlet	17.51	0	0.00	22.90	17.51
19.30					0.00	1.30		19.74	Weir	19.74					0.00	75.60	Inlet	19.74	0	0.00	23.00	19.74
19.40					0.00	1.40		22.06	Weir	22.06					0.00	76.00	Inlet	22.06	0	0.00	23.10	22.06
19.50					0.00	1.50	25.02	24.47	Weir	24.47	0.00	0.00	0.00	Weir	0.00	76.40	Inlet	24.47	0	0.00	23.20	24.47
19.60					0.00	1.60	26.64	26.96	Orifice	26.64	0.10	24.36	1.68	Weir	1.68	76.70	Inlet	28.32	0	0.00	23.30	28.32
19.70					0.00	1.70	28.16	29.52	Orifice	28.16	0.20	34.45	4.77	Weir	4.77	77.10	Inlet	32.92	0	0.00	23.40	32.92
19.80					0.00	1.80	29.60	32.17	Orifice	29.60	0.30	42.20	8.75	Weir	8.75	77.50	Inlet	38.36	0	0.00	23.50	38.36
19.90					0.00	1.90	30.98	34.88	Orifice	30.98	0.40	48.72	13.48	Weir	13.48	77.90	Inlet	44.46	0	0.00	23.60	44.46
20.00					0.00	2.00	32.30	37.67	Orifice	32.30	0.50	54.48	18.84	Weir	18.84	78.20	Inlet	51.14	0	0.00	23.70	51.14
20.00					0.00	2.00	32.30	31.01	Office	32.30	0.50	54.40	10.04	vveii	10.04	10.20	IIIIet	31.14	U	0.00	23.70	31.14

20.0

Ponds ABC HEC-HMS

Drainage Area	Area (ac)	CN	Lag Time (min)		
Ponds ABC Ex	14.0	82	9.8		
Ponds ABC DA	26.6	60	23.0		

Project: PP D Pond Simulation Run: 1000-Yr, 24-hour

Reservoir: Pond ABC (non-breach)

Start of Run: 17Apr2017, 00:00 Basin Model: PP D
End of Run: 20Apr2017, 00:01 Meteorologic Model: 1000-Yr
Compute Time: DATA CHANGED, RECOMPUTE Control Specifications: 72-Hr

Volume Units: O IN AC-FT

Computed Results

Peak Inflow:301.19 (CFS)Date/Time of Peak Inflow:17Apr2017, 12:05Peak Discharge:0.00 (CFS)Date/Time of Peak Discharge: 17Apr2017, 00:00Inflow Volume:31.44 (AC-FT)Peak Storage:31.44 (AC-FT)Discharge Volume:0.00 (AC-FT)Peak Elevation:10.39 (FT)

Established in 1960, Golder Associates is a global, employee-owned organization that helps clients find sustainable solutions to the challenges of finite resources, energy and water supply and management, waste management, urbanization, and climate change. We provide a wide range of independent consulting, design, and construction services in our specialist areas of earth, environment, and energy. By building strong relationships and meeting the needs of clients, our people have created one of the most trusted professional services organizations in the world.

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